

# APPLICATION UNDER UNITED STATES PATENT LAWS

Atty. Dkt. No. PW 279139  
(M#)

Invention: IMPROVED STRUCTURE OF GAS SENSOR

Inventor (s): HIBINO, Hideki and MIYAMOTO, Toshimi

Pillsbury Winthrop LLP  
Intellectual Property Group  
1100 New York Avenue, NW  
Ninth Floor  
Washington, DC 20005-3918  
Attorneys  
Telephone: (202) 861-3000

## This is a:

- ☐ Provisional Application
- ☒ Regular Utility Application
- ☐ Continuing Application  
☐ The contents of the parent are incorporated by reference
- ☐ PCT National Phase Application
- ☐ Design Application
- ☐ Reissue Application
- ☐ Plant Application
- ☐ Substitute Specification  
Sub. Spec Filed \_\_\_\_\_  
in App. No. \_\_\_\_\_ / \_\_\_\_\_
- ☐ Marked up Specification re  
Sub. Spec. filed \_\_\_\_\_  
In App. No. \_\_\_\_\_ / \_\_\_\_\_

## SPECIFICATION

## IMPROVED STRUCTURE OF GAS SENSOR

## BACKGROUND OF THE INVENTION

## 1 Technical Field of the Invention

The present invention relates generally to an improvement on  
5 a gas sensor which may be employed in an oxygen measuring device  
of an air-fuel ratio control system measuring an oxygen content in  
exhaust gasses of an internal combustion engine of automotive  
vehicles.

## 2 Background Art

10 For burning control of fuel in internal combustion engines,  
modern automotive vehicles use a gas sensor, e.g., as an oxygen  
sensor which is installed in an exhaust system to measure the  
concentration of oxygen in exhaust gasses.

European Patent Application EP 0918215 A2 teaches an  
15 oxygen sensor designed to define an air gap between an insulation  
porcelain and a metallic cover which is large enough for admitting  
air used as a reference gas in determining the concentration of  
oxygen. Fig. 21(a) illustrates the insulation porcelain disclosed in  
this application. The insulation porcelain 9 consists of a  
20 large-diameter portion 92 and a small-diameter portion 91. The  
small-diameter portion 91 is of a rectangular shape and has formed  
therein through holes 30 within which lead lines are held. The  
insulation porcelain 9 is fitted within a metallic cover (not shown) to  
define the air gap between an inner wall of the metallic cover and the  
25 small-diameter portion 91.

The formation of the insulation porcelain 9, however, experiences, as shown in Fig. 21(b), the deformation of the small-diameter portion 91 in compressing the ceramic powder because the interval O between an outer wall 911 of the small-diameter portion 91 and an outer wall 921 of the large-diameter portion 92 varies in a circumferential direction of the insulation porcelain 9, thus resulting in a decreased strength of the insulation porcelain 9. This problem is common to gas sensors of the type having a reference gas chamber admitting a reference gas used in determining the concentration of a specific gas.

#### SUMMARY OF THE INVENTION

It is therefore a principal object of the invention to avoid the disadvantages of the prior art.

It is another object of the invention to provide an improved structure of a gas sensor capable of admitting a sufficient amount of a reference gas into a reference chamber without scarifying the strength of an insulation porcelain.

According to one aspect of the invention, there is provided an improved structure of a gas sensor designed to measure a given component content in a gas. The gas sensor comprises: (a) a housing; (b) a sensing unit having a length disposed in the housing, the sensing unit having defined in a first end portion thereof a reference gas chamber to be filed with a reference gas used in providing a sensor signal through a lead which is employed in determining the given gas component content in the gas; (c) a first

metallic cover installed on the housing to cover a second end portion of the sensing unit; (d) a second metallic cover installed on a periphery of the first metallic cover; (e) a first vent formed in the first metallic cover; (f) a second vent formed in the second metallic cover  
 5 which communicates with the first vent to admit the reference gas into the reference gas chamber through a reference gas passage; and (g) an insulating member disposed in the first metallic cover, having formed therein a hole through which the lead passes to connect with the sensing unit, the insulating member being made of a cylindrical  
 10 porcelain having an outer peripheral wall which is substantially circular in cross section and which defines the reference gas passage.

In the preferred mode of the invention, the insulating member has a first end surface and a second end surface opposed to the first end surface in a longitudinal direction of the gas sensor  
 15 parallel to the length of the sensing unit. The insulating member has a through hole extending in a direction of the first end surface to the second end surface to define a portion of the reference gas passage.

20 The insulating member is arranged in alignment with the sensor unit and has a groove formed in the outer peripheral wall which extends from the first vent to the first end surface to define a portion of the reference gas passage.

The insulating member has a small-diameter portion formed  
 25 closer to the first end surface and a large-diameter portion continuing from the small-diameter portion. If a length of the

small-diameter portion in a direction is defined as  $L1$ , a distance  $L2$  between the large-diameter portion and an upstream end of the groove facing the first vent lies within a range of  $L1/5$  to  $L1/2$ .

The first vent has a diameter  $R$  in the longitudinal direction of the gas sensor. The distance between a point on a periphery of the first vent closest to the second end surface of the insulating member and an upstream end of the groove facing the first vent is greater than or equal to  $R/3$ .

The insulating member may alternatively have a groove formed in the outer peripheral wall which extends from the first vent to the second end surface to define a portion of the reference gas passage.

If a plane tangent to a periphery of the insulating member is defines as  $P$ , a plane passing through the deepest point of the groove in parallel to the plane  $P$  is defined as  $P1$ , and a plane passing in parallel to the plane  $P$  through the center of the through hole formed in the insulating member is defined as  $P2$ , a distance  $S1$  between the planes  $P$  and  $P1$  is smaller than or equal to a distance  $S2$  between the planes  $P$  and  $P2$ .

If a width of the reference gas passages defined on the outer peripheral wall of the insulating member is defined as  $H1$ , and a diameter of the insulating member is defined as  $H2$ , they are so selected as to meet a condition of  $H1 \leq H2 / 2^{1/2}$ .

The insulating member may alternatively have formed therein a plurality of lead holes through which leads pass to connect with the sensing unit. The reference gas passage may be defined at

a location where a line passing through a center of the insulating member between adjacent two of the lead holes intersects the outer peripheral wall of the insulating member.

The reference gas passage may alternatively be defined by a  
 5 hole formed in the insulating member which extends from a portion of the outer peripheral wall of the insulating member facing the first vent and communicates with the hole through which the lead passes.

The insulating member may have formed therein a lateral  
 10 hole extending between the lead holes in communication with the through hole extending in the direction of the first end surface to the second end surface of the insulating member to define the reference gas passage.

The reference gas passage may alternatively be defined by a  
 15 through hole formed in the insulating member which extends from a portion of the outer peripheral wall facing the first vent to the chamber through the small-diameter portion and the large-diameter portion.

The reference gas passage may alternatively be defined by an  
 20 inner wall of the first metallic cover and a surface of the outer peripheral wall of the insulating member tapering off to the first end surface.

The reference gas passage may alternatively be defined by an  
 inner wall of the first metallic cover and a first and a second annular  
 25 step formed on the outer peripheral wall of the insulating member. The first annular step is smaller in diameter than the second step.

## BRIEF DESCRIPTION OF THE DRAWINGS

The present invention will be understood more fully from the detailed description given hereinbelow and from the accompanying drawings of the preferred embodiments of the invention, which,  
5 however, should not be taken to limit the invention to the specific embodiments but are for the purpose of explanation and understanding only.

In the drawings:

Fig. 1 is a longitudinal sectional view which shows an oxygen  
10 sensor equipped with an insulating holder according to the first embodiment of the invention;

Fig. 2 is a partially enlarged view which shows a structure of an insulating holder of the first embodiment;

Fig. 3(a) is a horizontal sectional view taken along the line  
15 A-A in Fig. 3(b);

Fig. 3(b) is a longitudinal sectional view which shows reference gas passages defined in an insulating holder of the first embodiment;

Fig. 4 is a horizontal sectional view which shows an  
20 insulating holder of the first embodiment;

Fig. 5 is a longitudinal sectional view which shows another type of oxygen sensor equipped with an insulating holder in the first embodiment;

Fig., 6(a) is a lateral sectional view which shows a  
25 modification of the insulating holder of Fig. 4;

Fig. 6(b) is a lateral sectional view which shows another modification of the insulating holder of Fig. 4;

Fig. 7 is a partially vertical sectional view which shows reference gas passages of a gas sensor according to the second  
5 embodiment of the invention;

Fig. 8 is a lateral sectional view which shows reference gas passages of a gas sensor according to the third embodiment of the invention;

Fig. 9 shows a test machine used for measuring the strength  
10 of an insulating holder of the gas sensor in Fig. 8;

Fig. 10 is a graph which shows the strength of the insulating holder in Fig. 8;

Fig. 11 is a graph which shows the strength of the insulating holder in Fig. 8 for different values of  $S1$ ;

Fig. 12 is a graph which shows the strength of the insulating  
15 holder in Fig. 8 for different values of  $H1$ ;

Fig. 13(a) is a horizontal sectional view taken along the line  $B-B$  in Fig. 13(b);

Fig. 13(b) is a longitudinal sectional view which shows  
20 reference gas passages defined in an insulating holder according to the fourth embodiment of the invention;

Fig. 14(a) is a horizontal sectional view taken along the line  $C-C$  in Fig. 14(b);

Fig. 14(b) is a longitudinal sectional view which shows  
25 reference gas passages defined in an insulating holder of the fifth embodiment;



Fig. 15(a) is a horizontal sectional view taken along the line *D-D* in Fig. 15(b);

Fig. 15(b) is a longitudinal sectional view which shows reference gas passages defined in an insulating holder which is a  
5 modification of the one shown in Figs. 14(a) and 14(b);

Fig. 16 shows a modification of the fourth embodiment in Figs. 13(a) and 13(b);

Figs. 17(a), 17(b), and 17(c) show modifications of reference gas passages, as shown in Figs. 14(a), 14(b), 15(a), 15(b), and 16;

10 Fig. 18(a) is a horizontal sectional view taken along the line *E-E* in Fig. 18(b);

Fig. 18(b) is a longitudinal sectional view which shows reference gas passages defined in an insulating holder of the sixth embodiment of the invention;

15 Figs. 19(a) and 19(b) show an insulating holder according to the seventh embodiment of the invention;

Fig. 20 shows an insulating holder according to the eighth embodiment of the invention; and

Fig. 21(a) is a plan view which shows a conventional  
20 insulating holder installed in an oxygen sensor; and

Fig. 21(b) is a side view which shows the insulating holder of Fig. 21(a) which is deformed during a production process.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring to the drawings, wherein like reference numbers  
25 refer to like parts in several views, particularly to Fig. 1, there is

shown an oxygen sensor 1 according to the first embodiment of the invention which may be employed in an air-fuel ratio control system for automotive vehicles. Note that the present invention is not limited to an oxygen sensor and may alternatively used with a  
5 variety of gas sensors such as HC, CO, and NOx sensors.

The oxygen sensor 1 generally includes a housing 10, a sensing unit 2, and signal leads 291 and 292 connected to the sensing unit 2. The signal leads 291 and 292 provide sensor signals to an external device which are used, as will be described  
10 later in detail, in determining the concentration of oxygen contained in a gas. The sensing unit 2 has formed therein a reference gas chamber 250 into which a reference gas (i.e., air) is admitted for use in providing the sensor signals through the signal leads 291 and 292. This technique is well known in the art, and explanation thereof in  
15 detail will be omitted here. For instance, U.S. application No. 09/196,693, filed on November 20, 1998, assigned to the same assignee as that of this application teaches a gas measuring method in this type of gas sensor, and disclosure of which is incorporated herein by reference.

The oxygen sensor 1 also includes a first metallic cover 11 and a second metallic cover 12. The first metallic cover 11 covers a base portion of the sensing unit 2 and is fitted in an end of the housing 10. The second metallic cover 12 is disposed around an upper portion of the first metallic cover 11, as viewed in the drawing.  
20 The first and second metallic covers 11 and 12 have formed therein first and second air vents 110 and 120 in alignment with each other  
25

for admitting the reference gas into the reference gas chamber 250.

An insulating holder 3 is, as clearly shown in Fig. 2, disposed inside the first metallic cover 11 which has formed therein through holes 30 into which the leads 191 and 192 are inserted. The  
 5 insulating holder 3 is made of a hollow cylindrical insulation porcelain and defines reference gas passages 35 between an outer wall 311 and an inner wall of the first metallic cover 11 which lead to the reference gas chamber 250.

The sensing unit 2 is, as shown in Fig. 1, retained within the  
 10 housing 11. The sensing unit 2 and the housing 11 are hermetically sealed.

The first metallic cover 11 consists of two cover members: outer and inner cover members 111 and 112. The inner cover member 112 is joined at an end to an upper end of the housing 10  
 15 through a caulking ring 119. The outer cover member 111 is joined to an upper portion of the inner cover member 112 by crimping.

The inner cover member 112 has an open end 116, as shown in Fig. 2, abutting on a lower surface 328 of a large-diameter portion 32 (i.e., a flange) of the insulating holder 3 to retain the insulating  
 20 holder 3 within the first metallic cover 11 against a spring pressure of a spring 117 disposed between an upper surface 329 of the large-diameter portion 32 and a shoulder 118 of the outer cover member 111.

A sealing member 14 is fitted in an upper end of the inner  
 25 cover member 112 through which the leads 191, 192, and 251 pass.

The insulating holder 3, as clearly shown in Figs. 3(a) and

3(b), has formed therein four through holes 30 through which signal pickup leads 291 and 292, a pair of leads 259 connected to a heater 25, as will be described later in detail, the leads 191 and 192, and a pair of leads 251 pass. The leads 291, 292, and 259 are connected  
 5 to the leads 191, 192, and 251 through connectors 195 within the through holes 30, respectively. Note that another pair of leads passes through the insulating holder 3, but it is located in an invisible area of the drawing and omitted here.

The insulating holder 3 has formed in an a lower portion  
 10 thereof, as shown in Fig. 3(b), a cavity 309 to which all the through holes 30 are exposed and in which a base portion of the sensing unit 2 is disposed.

The insulating holder 3, as shown in Figs. 3(a) to 4, includes the large-diameter portion 32, a small-diameter portion 31, and a tip  
 15 portion 33. The tip portion 33 projects from the large-diameter portion 32 toward the tip of the sensing unit 2 and is smaller in diameter than the large-diameter portion 32. These portions 31, 32, and 33 have circular sections, as clearly shown in Fig. 4. The large-diameter portion 32 and the small-diameter portion 31 are  
 20 arranged coaxially, so that the interval between an outer wall 321 of the large-diameter portion 32 and an outer wall 311 of the small-diameter portion 31 is kept constant in a circumferential direction of the insulating holder 3. This eliminates the problem encountered in the prior art structure, as shown in Figs. 21(a) and  
 25 21(b), that the insulating porcelain 9 is deformed during a production process.

The reference gas passages 35 are, as can be seen from Figs. 3(a) and 4, defined between the inner wall of the outer cover member 111 and four grooves 160 provided in an outer wall 311 of the small-diameter portion 31 of the insulating holder 3. The grooves 160 each have an arc-shaped cross section and are, as shown in Fig. 3(a), formed at locations where lines *T* passing through the center of the insulating holder 3 between adjacent two of the through holes 30 intersect the outer wall 311 of the small-diameter portion 31. This allows the small-diameter portion 31 to have wider round outer surfaces formed at regular intervals in the circumferential direction of the insulating holder 3, thus resulting in an improved strength as compared with the prior art structure shown in Figs. 21(a) and 21(b). Each of the reference gas passages 35 extends vertically, as viewed in Fig. 3(b), from one of the first air vents 110 to a base end 301 of the insulating holder 3.

The insulating holder 3 also has a central passage 39 extending along a longitudinal center line thereof which opens into the cavity 309.

The second metallic cover 12 is installed on the periphery of the upper portion of the first metallic cover 11 and is crimped to form, as shown in Fig. 2, two annular joints 161 and 162 to the first metallic cover 11 for retaining a water-repellent filter 13 between the first and second metallic covers 11 and 12. Specifically, the first metallic cover 11, the second metallic cover 12, and the water-repellent filter 13 are connected fixedly to each other through the annular joints 161 and 162.

The sensing unit 2, as shown in Fig. 1, consists of a hollow cylindrical solid electrolyte body 20 with a bottom, a measuring electrode formed on an outer wall of the body 20 exposed to a gas chamber 150, and a reference electrode formed on an inner wall of the body 20 exposed to the reference gas chamber 250. This structure is known, for example, in European Patent Application EP 0918215 A2 assigned to the same assignee as that of this application, disclosure of which is incorporated herein by reference.

Within the reference gas chamber 250, a bar-shaped heater 25 is disposed which heats the measuring and reference electrodes up to a temperature at which the oxygen concentration can be measured correctly. The measuring and reference electrodes have conductive terminals connected to the signal pickup leads 291 and 292. The heater 25 is supplied with power through the leads 259.

In operation, the air 8 which is, as indicated by arrows in Fig. 3(b), introduced from the second air vents 120 to the first air vents 110 through the water-repellent filter 13 flows upward, as viewed in the drawing, in the reference gas passages 35 and reaches the base end 301 of the insulating holder 3. Next, the air 8 passes through a gap between the base end 301 and the bottom of the sealing member 14 and flows downward into the cavity 309 through the holes 30 and the central holes 39. The air 8 emerging from the lower end 302 of the insulating holder 3 enters the reference gas chamber 250 at the upper end of the sensing unit 2.

The oxygen sensor 1 of this embodiment is designed to measure an oxygen content in gasses using the oxygen

concentration dependent electromotive force or the limiting current. Specifically, the measurement of the oxygen content using the oxygen concentration dependent electromotive force is accomplished by monitoring through the measuring and reference electrodes the  
5 electromotive force produced in the solid electrolyte body 20 which depends upon a difference in oxygen concentration between the air 8 and the gas within the gas measuring chamber 150. The measurement of the oxygen content using the limiting current is accomplished by applying a given voltage across the measuring and  
10 reference electrodes to pick up a limiting current which depends upon the concentration of oxygen in the gasses. These techniques are known in the art, and explanation thereof in detail will be omitted here. The sensing unit 2 may alternatively be formed by laminations such as one shown in Fig. 5 in which the sensing unit 2  
15 is made of a laminated plate having a heater layer. Further, U.S.P. No. 5,573,650, issued on November 12, 1996 to Fukaya et al. teaches such a structure, disclosure of which is incorporated herein by reference.

The grooves 160 formed in the small-diameter portion 31 of  
20 the insulating holder 3 to define the reference gas passages 35 may alternatively be of generally rectangular configuration in cross section, as shown in Fig. 6(a), or have parallel steps, as shown in Fig. 6(b), defining an additional central groove.

Fig. 7 shows the second embodiment of the invention.

25 The reference gas passages 35 are, like the first embodiment, defined by the grooves 160 formed in the outer wall 311 of the

insulating holder 3, but each of the grooves 160 of this embodiment has a lower end 350 defining an inlet which leads to one of the first air vents 110 and which meets the following locational conditions.

Letting the length of the small-diameter portion 31 of the  
 5 insulating holder 3 and the distance between the upper surface 329 of the large-diameter portion 32 and the lower end 350 of each of the grooves 160 be  $L1$  and  $L2$ , respectively,  $L2$  lies within a range of  $L1/5$  to  $L1/2$ , preferably  $L1/3$ . For instance,  $L1 = 12.5\text{mm}$ , and  $L2 = 6\text{mm}$ . This allows the sensor to be decreased in size without  
 10 sacrificing the strength of the small-diameter portion 31 of the insulating holder 3.

The lower ends 350 face the first air vents 110, respectively. If the diameter  $R$  of each of the first air vents 110 is defined as  $R$ , and the distance between a lowermost portion of 119 of each of the first  
 15 air vents 110 and the lower end 350 of a corresponding one of the grooves 160 is defined as  $R1$ , then they are so selected as to meet a condition of  $R1 \geq R/3$ . For instance,  $R = 2\text{mm}$ , and  $R1$  is  $0.5\text{mm}$ . This ensures the admission of a sufficient amount of air (i.e., the reference gas) into the sensor.

20 Other arrangements are identical with those in the first embodiment, and explanation thereof in detail will be omitted here.

Fig. 8 shows the third embodiment of the invention.

The reference gas passages 35 are, like the first embodiment, defined by the grooves 160 formed in the outer wall 311 of the  
 25 insulating holder 3, but the grooves of this embodiment 160 are designed so as to meet the following geometrically conditions.



If a plane tangent to the outer wall 311 of the small-diameter portion 31 is defines as  $P$ , a plane passing through the deepest point  $M$  of each of the grooves 160 in parallel to the plane  $P$  is defined as  $P1$ , and a plane passing in parallel to the plane  $P$  through the center  $O1$  of one of the holes 30 located closest to the plane  $P$  is defined as  $P2$ , the distance  $S1$  between the planes  $P$  and  $P1$  is smaller than or equal to the distance  $S2$  between the planes  $P$  and  $P2$  ( $S1 \leq S2$ ). For instance,  $S1 = 1\text{mm}$ , and  $S2 = 2\text{mm}$ .

If the width of each of the reference gas passages 35 is defined as  $H1$ , and the diameter of the small-diameter portion 31 of the insulating holder 3 is defined as  $H2$ , they are so selected as to meet a condition of  $H1 \leq H2 / 2^{1/2}$ , preferably  $H1 \leq (2 \times H2) / 3$ . For instance,  $H1 = 3\text{mm}$ , and  $H2 = 10\text{mm}$ . Other arrangements are identical with those in the first embodiment, and explanation thereof in detail will be omitted here.

Strength tests were performed for a comparative test piece equivalent to the insulating holder 3 not having the grooves 60 in the small-diameter portion 31, the prior art insulation porcelain 9 shown in Fig. 21(a), and the insulating holder 3 of this embodiment using a test machine as shown in Fig. 9. The results of the tests are shown in Fig. 10.

The test machine has a table 80 on which a round bar 81 having a diameter of 5mm is retained, and a support surface 810 is formed. The insulating holder 3 is placed in contact of the small-diameter portion 31 and the large-diameter portion 32 with the round bar 81 and the support surface 810, respectively. A

round bar 82 having a diameter of 4mm is placed on the small-diameter portion 31 of the insulating holder 3. The pressure  $F$  which causes the insulating holder 3 to be deformed 0.05mm per minute is applied to the round bar 82 to measure the disruptive strength. The same tests were performed for the prior art insulation porcelain 9 and the comparative test piece.

The graph of Fig. 10 shows that the insulating holder 3 of this embodiment has a disruptive strength greater than that of the prior art insulation porcelain 9 closer to that of the comparative test piece.

The strength tests were also performed on the insulating holders 3 in which  $H1 = 3\text{mm}$ ,  $S2 = 2\text{mm}$ , and  $S1$  has different values. The results of the tests are indicated in a graph of Fig. 11. As shown by the graph, the disruptive strength of the insulating holder 3 is decreased greatly when  $S1$  exceeds  $S2$  ( $S1 > S2$ ).

The strength tests were also performed on the insulating holders 3 in which  $S1 = 0.5\text{mm}$ ,  $H2 = 10\text{mm}$ , and  $H1$  has different values. The results of the tests are indicated in a graph of Fig. 12. As shown by the graph, the disruptive strength of the insulating holder 3 is decreased greatly when  $H1$  exceeds  $H2 / 2^{1/2}$ .

Therefore, it is appreciated that the insulating holder 3 meeting the condition of  $S1 \leq S2$  and/or the condition of  $H1 \leq H2 / 2^{1/2}$  has an increased strength.

Figs. 13(a) and 13(b) show the fourth embodiment of the insulating holder 3.

The insulating holder 3 has four grooves, similar in shape to the grooves 160 in the first embodiment, which are formed in the

small-diameter portion 31 and the upper surface 329 and the side surface of the large-diameter portion 32 to define reference gas passages 36. Each of the grooves is made up of a vertical groove 361, a horizontal groove 362, and a vertical groove 363. The

5 vertical grooves 361 are formed in the side wall of the small-diameter portion 31 at regular intervals. The horizontal grooves 362 formed in the upper surface 329 of the large-diameter portion 32. The vertical grooves 363 are formed in the side wall of the tip portion 33. Each of the reference gas passages 36 extends from one of the first

10 air vents 110 to an annular gap defined between the tip portion 33 of the insulating holder 3 and the inner wall of the outer cover member 111. Other arrangements are identical with those in the first embodiment, and explanation thereof in detail will be omitted here.

Figs. 14(a) and 14(b) show the fifth embodiment of the

15 insulating holder 3.

The insulating holder 3 has four holes formed at regular intervals in the outer wall 311 thereof to define reference gas passages 37 extending horizontally, as viewed in Fig. 14(b). Each of the reference gas passages 37 establishes communication between

20 one of the first air vents 110 and one of the through holes 30. Other arrangements are identical with those in the first embodiment, and explanation thereof in detail will be omitted here.

Four holes, as shown in Figs. 15(a) and 15(b), which are greater in size than the through holes 30 may be formed at regular

25 intervals in the outer wall 311 thereof to define the reference gas passages 37 extending horizontally, as viewed in Fig. 15(b).

Fig. 16 shows a modification of the fifth embodiment in Figs. 14(a) and 14(b).

The insulating holder 3 has four holes defining reference gas passages 38. Each of the reference gas passages 38 extends from one of the air vent holes 110 to the central hole 39 between the adjacent two of the holes 30.

Each of the reference gas passages 37 and 38 in Figs. 14(a), 14(b), 15(a), 15(b), and 16 may have any of different sectional shapes as shown in Figs. 17(a), 17(b), and 17(c).

Figs. 18(a) and 18(b) show the insulating holder 3 according to the sixth embodiment of the invention.

The insulating holder 3 has formed therein four vertical holes which define reference gas passages 41. Each of the reference gas passages 41 extends from one of the first air vents 110 to the cavity 309 in the insulating holder 3. Specifically, each of the reference gas passages 41 is made up of two sections: one is defined by a groove formed in the outer wall 311 extending from one of the first air vents 110 to a corner between the small-diameter portion 31 and the large-diameter portion 32 and the inner wall of the outer cover member 111 and the other is defined by a slant hole extending inwardly from the corner between the small-diameter portion 31 and the large-diameter portion 32 to the cavity 309. Other arrangements are identical with those in the first embodiment, and explanation thereof in detail will be omitted here.

Figs. 19(a) and 19(b) show the insulating holder 3 according to the seventh embodiment of the invention.

The insulating holder 3 has an annular step 42 formed around the outer wall 311 of the small-diameter portion 31 to define an upper annular passage 170 and a lower annular passage 175 between the outer wall 311 and the inner wall of the outer cover member 111. Specifically, the upper annular passage 170 is greater in volume than the lower annular passage 175. The lower annular passage 175 directs the air 8 admitted from the first air vents 110 to the upper annular passage 170. The upper annular passage 170 directs the air 8 into the holes 30 and the central hole 39 through the base end 301 of the insulating holder 3. Other arrangements are identical with those in the first embodiment, and explanation thereof in detail will be omitted here.

Fig. 20 shows the insulating holder 3 according to the eighth embodiment of the invention.

The insulating holder 3 has a tapered wall 43 formed on the small-diameter portion 31 to define an annular passage 180 between itself and the inner wall of the outer cover member 111. The annular passage 180 increases in volume toward the base end 301 of the insulating holder 3 and directs the air admitted from the first air vents 110 into the holes 30 and the central hole 39 through the base end 301. Other arrangements are identical with those in the first embodiment, and explanation thereof in detail will be omitted here.

The above second to eighth embodiments may be used with the oxygen sensor shown in Fig. 1 or 5. Some of the first to eighth embodiments may be combined to form two or more types of

reference gas passages in the insulating holder 3.

While the present invention has been disclosed in terms of the preferred embodiments in order to facilitate better understanding thereof, it should be appreciated that the invention  
5 can be embodied in various ways without departing from the principle of the invention. Therefore, the invention should be understood to include all possible embodiments and modifications to the shown embodiments which can be embodied without departing from the principle of the invention as set forth in the  
10 appended claims.